Designer’s
NOTEBOOK
STONE VENEER-FACED PRECAST
Stone Veneer-Faced Precast Offers Cost Efficiencies

Natural stone has been used widely in building construction for centuries due to its strength, durability, aesthetic effect, availability and inherent low costs for maintenance. In the 1960s, the practice of facing skeleton-frame structures with large prefabricated concrete components to decrease construction time and reduce costs resulted in a combination of the rich beauty of natural stone veneer and the strength, versatility and economy of precast concrete.

Stone veneer-faced precast concrete panels offer many benefits. These include:

1. Veneer stock can be used in thinner sections because anchoring points may be placed closer together.

2. Multiplane units such as column covers, spandrels with integral soffit and sill sections, deep reveal window frames, inside and outside corners, projections and setbacks, and parapet sections are more economically assembled as veneer units on precast concrete panels (Fig. 1).

3. Precast concrete backup systems permit faster enclosure, allowing earlier work by other trades and subsequent earlier occupancy, because each of the larger panels incorporate a number of veneer pieces.

4. Veneered precast concrete panels can be used to span column-to-column, thereby reducing floor-edge loading and eliminating elaborate temporary scaffolding.

The purchaser of the stone should appoint a qualified individual to be responsible for coordination. This person should oversee delivery and scheduling responsibility and should ensure acceptable color uniformity. Color control or blending of the stone veneer should take place at the stone fabricator’s plant, where ranges of color and shade, finishes and markings such as veining, seams and intrusions are viewed most easily. Acceptable stone color should be judged for an entire building elevation rather than as individual panels. The responsibility for stone coordination should be written into the specifications so its cost can be bid. The owner, architect and precaster should visit the stone fabricator’s plant to view the stone veneer and establish criteria and methods for color range blending on the project.

Separate subcontracts and advance awards often occur in projects with stone-veneered panels. While these procedures may affect normal submission routines, it is not intended that responsibilities for accuracy should be transferred or reassigned. The precaster is responsible for precast concrete details and dimensions, while the stone-veneer fabricator is responsible for stone details, dimensions and drilling of anchor holes.
The production of stone veneer panels requires adequate lead time in order to avoid construction delays. Therefore, it is important that approvals for shop drawings are obtained expeditiously. Furthermore, it is recommended that the designer allow the submission of shop drawings in predetermined stages so manufacturing can begin as soon as possible and ensure there is a steady and timely flow of approved information to allow uninterrupted fabrication.

The precast concrete producer must provide the stone quantity and sequence requirements to meet the erection sequences. The precaster and stone fabricator should coordinate packaging requirements to minimize handling and breakage. Extra stone (approximately 2 to 5 percent) should be supplied to allow immediate replacement of damaged stone pieces, particularly if the stone is not supplied from a domestic source.

Because of the difference in material properties between natural stone and concrete, veneered panels are more susceptible to bowing than all-concrete units. However, panel manufacturers have developed design and production procedures to minimize bowing.

The panel manufacturer and designer should consider the following in design and production in order to minimize or eliminate panel bowing:

1. The temperature differential (exterior to interior).
2. Coefficients of expansion of the materials.
3. Ratio of cross-sectional areas of the materials and their moduli of elasticity.
4. Amount, location and type of reinforcement in the concrete panel.
5. The use of prestressing.
6. Type and location of connections to the structure.
7. Rigidity of connection between stone veneer and concrete backup (too rigid may cause problems).
8. Shrinkage of the concrete.

Minimum thickness of backup concrete on flat panels that will control bowing or warping is usually 5 to 6 inches, but 4 inches has been used where the panel is small, or it has adequate rigidity obtained through panels shape or thickness of natural stone. See Fig. 2 for mold considerations. Cover depth of reinforcement must be a minimum of 3/4 inch at the veneer surface. Non-corrosive spacers such as plastic should maintain this cover.

Stone Strength

The strength of natural stone depends on several factors: the size, rift and cleavage of crystals, the degree of cohesion, the interlocking geometry of crystals, the nature of natural cementing materials present and the type of crystal. The stone's properties will vary with the locality from which it is quarried. Therefore, it is important that current testing is performed for stone quarried for a specific project.

Sedimentary and metamorphic rocks, such as limestone and marble, will exhibit different strengths when measured parallel and perpendicular to their original bedding planes. Igneous
rocks, such as granite, may or may not exhibit relatively uniform strength characteristics on the various planes. In addition, the surface finish, freezing and thawing, and large temperature fluctuations will affect the strength and in turn influence the anchorage system. Information on the durability of the specified stone should be obtained through current testing in conjunction with observations of existing installations of that particular stone. This information should include such factors as tendency to warp, reaction to weathering forces, resistance to chemical pollutants, resistance to chemical reaction from adjacent materials and reduction in strength from the effects of weathering or wetting and drying.

Prior to awarding the precast concrete contract, tests should be performed to determine the physical properties of the stone being considered. The testing should be done on stone with the same finish and thickness to be used on the structure. Flexural tests (ASTM C880) should be used to evaluate the physical properties and obtain design values. Absorption testing (ASTM C97) helps evaluate freeze-thaw durability. These properties, along with properties of the anchor system, should be used to ensure adequate strength of the panel to resist loads during handling, transportation, erection and in-service conditions.

Stone veneers used for precast facing are usually thinner than those used for conventionally set stone, with the maximum size generally determined by the stone strength. Table 1 summarizes typical dimensions. Veneers thinner than those listed can result in anchors being reflected on the exposed surface, excessive breakage or permeability problems.

The length and width of veneer materials should be sized to a tolerance of $+0 - 1/8$ inch, since a plus tolerance can present problems on precast concrete panels. This tolerance becomes important when trying to line up the false joints on one panel with those on the panel above or below, particularly when there are a large number of pieces of stone on each panel. Tolerance
allowance for out-of-square is
± 1/16-inch difference in length of
the two diagonal measurements.

Flatness tolerances for
finished surfaces depend on the
type of finish. For example, the
granite industry’s flatness
tolerances vary from 3/64 inch for a polished surface to 3/16 inch for flame (thermal) finish
when measured with a 4-foot straight edge. Thickness variations are less important, since
concrete will provide a uniform back face except at corner butt joints. In such cases, the
finished edges should be within ± 1/16 inch of the specified thickness. However, large thickness
variations may lead to the stone being encased with concrete and thus restrict relative
movement of the materials. The aesthetic problems that occur with tolerances concern the
variation from a flat surface on an exposed face and stone pieces being out of square.

The stone fabricator or precaster appear to have the dominant responsibility for conducting
the anchor tests, with the architect or engineer of record occasionally determining the type of
anchorage. However, it is preferable for the architect to determine anchor spacing so that
common information can be supplied to all bidders (refer to ASTM C1242). Contract
documents should define clearly who drills the anchor holes in the stone; type, number and
location of anchors; and who supplies the anchors. In most cases, the stone fabricator drills
the anchor holes in the stone using a diamond-core bit with a non-pneumatic tool.

It is recommended that the precaster detail all precast units to the point where the fabri-
cator of the veneer is able to incorporate details, sizes and anchor holes for the individual
stone pieces.

It also is recommended that there be no bonding between stone veneer and concrete backup
in order to minimize bowing, cracking and staining of the veneer. Flexible mechanical anchors
should be used to secure the veneer.

Two methods may be used to prevent bond between the veneer and concrete to allow for
independent movement: a 6-mil polyethylene sheet or a closed-cell, 1/8- to 1/4-inch
polyethylene foam pad. Using a compressible bondbreaker is preferred because it allows
movement of stones with uneven surfaces, either of individual pieces or between stone pieces
on a panel.

Preformed anchors, 1/8- to 5/8-inch in diameter, fabricated from Type 304 stainless steel,
are supplied by the stone fabricator or, in some cases, by the precaster depending on the
contract document requirements. The number and location of anchors should be determined
by a minimum of five shear and tension tests conducted on a single anchor embedded in a

<table>
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<th>Material</th>
<th>Minimum recommended thickness (in.)</th>
<th>Length range (ft.)</th>
<th>Width range (ft.)</th>
<th>Maximum area (ft²)</th>
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<td>15</td>
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</tbody>
</table>

* Surface voids filled front and back

Five Fremont Center in San Francisco is clad with 1 1/4-and
2-inch-thick travertine-faced
precast concrete panels.
(Architect: Skidmore, Owings & Merrill)
stone/precast concrete test sample using ASTM E488 or ASTM C1354 and the anticipated applied loads, both normal and transverse to the panel. Care should be taken in grasping the anchor.

Design of anchorage and size of the stone should be based on specific test values for the actual stone to be installed. Test samples for anchor tests should be a typical panel section of about 1 square foot and approximate as closely as possible actual panel anchoring conditions. A bondbreaker should be placed between stone and concrete during sample manufacture to eliminate any bond between veneer and concrete surface. Depending on the size of the project, it may be desirable to perform shear and tensile tests of the anchors at intervals during the fabrication period.

Four anchors usually are used per stone piece, with a minimum of two recommended. The number of anchors has varied from one per 1 1/2 square foot of stone to one per 6 square feet, with one per 2 to 3 square feet being the most common. Anchors should be 6 to 9 inches from an edge with not more than 24 to 30 inches between anchors depending on the local building code. The shear capacity of the spring clip (hairpin) anchors perpendicular to the anchor legs is greater than when they are parallel, and capacity depends on the strength of the stone. A typical marble veneer anchor detail with a toe-in spring clip (hairpin) anchor is shown in Fig. 3, while a typical granite veneer anchor detail is shown in Fig. 4. The toe-out anchor in granite may have as much as 50 percent more tensile capacity than a toe-in anchor, depending on the stone strength.

Depth of anchor holes should be approximately half the thickness of the veneer (minimum depth of 3/4 inch). Minimum concrete cover over the drilled hole should be 3/8 inch to avoid spalling during drilling and spotting from absorbed moisture. The hole should be drilled at an angle of 30 to 45 degrees to the plane of the stone. Holes 1/16 inch larger than the anchor are common, as excessive looseness reduces holding power. Anchor holes should be within ± 3/16 inch of the specified hole spacing, particularly for the spring clip anchors.
Stainless-steel dowels, smooth or threaded, may be installed to a depth of two-thirds of the stone thickness, with a maximum depth of 2 inches at 45- to 60-degree angles to the plane of the stone. The minimum embedment in the concrete backup to develop the required bond length is shown in Fig. 5. Dowel size varies from 3/16 to 5/8 inch for most stones, except that it varies from 1/4 to 5/8 inch for soft limestone and sandstone and depends on thickness and strength of stone.

Limestone traditionally has been bonded and anchored to the concrete, because it has the lowest coefficient of expansion. Limestone also has been used traditionally in thicknesses of 3 to 5 inches, but it is now being used as thin as 1 3/4 inches. If limestone is to be bonded, use a moisture barrier/bonding agent on the backside of the stone to eliminate the possibility of staining the stone veneer with alkali salts in the concrete. When limestone is 2 inches or thinner, use a bondbreaker along with mechanical anchors. Dowels and spring-clip anchors can be used to anchor limestone. Typical dowel details for limestone veneers are shown in Figs. 5 and 6. The dowels in Fig. 6 should be inserted at opposing angles to secure stone facing to the backup concrete.

Some flexibility should be introduced with all anchors by minimizing the anchor's diameter, to allow for the inevitable relative movements that occur with temperature variations and concrete shrinkage. Unaccommodated relative movements can result in excessive stress problems and eventual failure at an anchor location. Depending on the size of the project, consideration may be given to accelerated cyclic temperature tests to determine the effects on the anchors.

Some designers use two-part polyester or epoxy to fill the anchor holes in order to eliminate intrusion of water into the holes and to prevent the possible dark, damp appearance of moisture on the exposed stone surface. The polyester or epoxy increases the

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**Fig. 5** Typical cross anchor dowels for stone veneer

**Fig. 6** Typical anchors for limestone veneer
shear capacity and rigidity of the anchors. The rigidity may be partially overcome by using 1/2-inch-long compressible (60 durometer) rubber or elastomeric grommets or sleeves on the anchor at the back surface of the stone, as seen in Fig. 7.

Differential thermal expansion of the stone and unfilled epoxy may cause cracking of the stone veneer. The coefficient of expansion of epoxy and stone should closely match. It may be more desirable to fill the anchor hole with a low modulus polyurethane sealant. The overall effect of either epoxy or sealant materials on the behavior of the entire veneer should be evaluated prior to their use. At best, the long-term service of epoxy is questionable, so any increase in shear value should not be used in calculating long-term anchor capacity.

The stone trade associations and the suppliers of different kinds of building stones recommend safety factors. Because of the expected variation in the physical properties of natural stones and the effects of weathering, recommended safety factors are larger than those used for manufactured building materials, such as steel and concrete. The minimum recommended safety factor, based on the average of the test results, is 4 for anchorage components. If the range of test values exceeds the average by more than ±20 percent, then the safety factor should be applied to the lower bound value. (See Appendix to ASTM C1242 for a discussion on safety factors.)

Finite-element analysis is a useful technique for evaluating stress in a veneer panel system. This necessitates testing to determine the spring constant values for the panel's material components to model the assembly. Stone veneer should be tested in flexure, (ASTM C1352). The section properties and modulus of elasticity also should be determined. Granite rift (bedding) planes, direction and grain size influence modulus of elasticity. Shear and tensile tests are required for the anchors. The spring constant of a compressible bondbreaker should be determined. For insulation, compressive-spring and shear-spring constants should be determined if no bondbreaker is used.

COMING NEXT ISSUE: More on stone veneer-faced precast, including the unique perspective of a practicing architect.